

# The CNES Intercalibration Method over Desert Sites

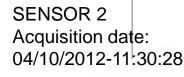
Sophie Lachérade

# CONTENT

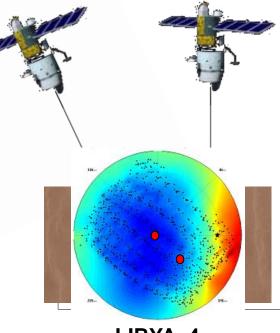
- Context
- Approach description
- Matchup Strategy
- Atmospheric corrections
- Interpolation strategy
- Improvement



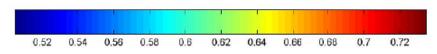
#### Why is it difficult to inter-calibrate two sensors over desert sites:



SENSOR 1 Acquisition date: 04/07/2012-11:16:24



#### LIBYA\_4



#### **Different Acquisition Date**

Is the same site (position, spectral and bidirectional behaviour) between S1 and S2?

What about the atmosphere content?
How to take into account the difference in AOT?

#### **Different Acquisition Time**

The sun position is not the same How to take into account the difference of the atmosphere contribution ? [ $\theta s(S1) = 12.90 \degree - \theta s(S2) = 27.25 \degree$ ]

#### **Different viewing conditions**

[ 
$$\theta v(S1)=0^{\circ} - \theta v(S2)=25^{\circ}$$
 ] is  $\rho_{\theta i, \theta v, \Delta \phi}(S1)=\rho_{\theta i, \theta v, \Delta \phi}(S2)$  ?





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What about the atmosphere content?
How to take into account the difference in AOT?

Libya\_4 have been chosen for its time stability and homogeneity

No information about AOT
Use of statistics to overcome this issue (SADE)

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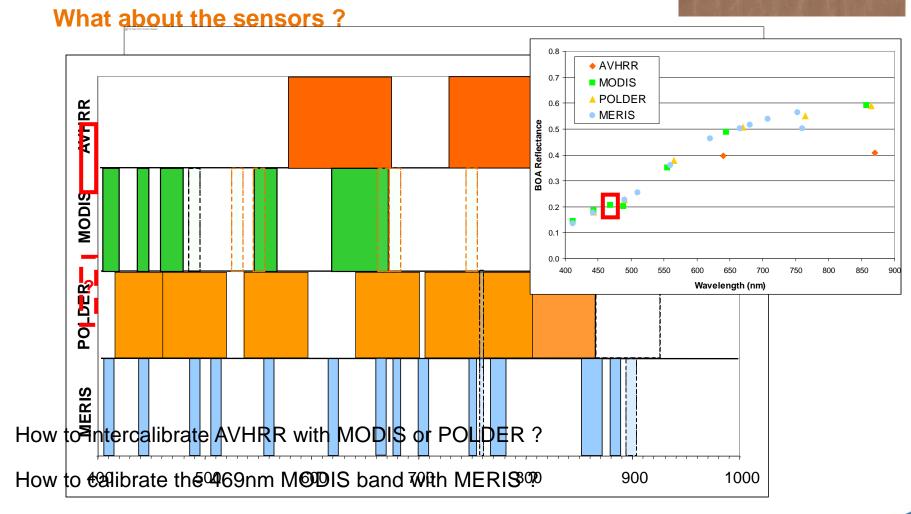
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$$\theta v(S1)=0^{\circ} - \theta v(S2)=25^{\circ}$$
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Matching conditions between \$1 and \$2 to limit the bidirectional effects of the site

Processing to compute the S1 into the geometry of the acquisition S2





How to take into account the difference between the sensors spectral response?

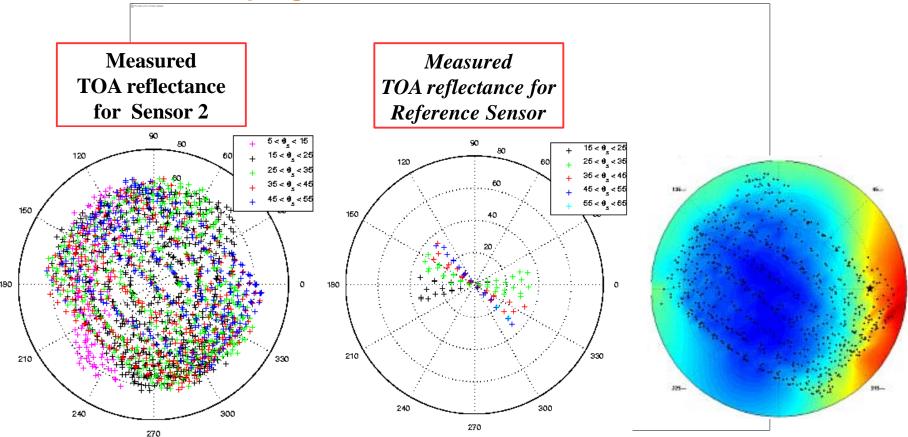
→ Use of interpolation functions



Overview of the CNES inter-calibration method **Cross-calibration** Sensor 2 vs Reference Sensor Comparison =  $\Delta A_{k}$ Measured Measured **Computed TOA reflectance** TOA reflectance for **TOA reflectance** for Sensor 2 Reference Sensor for Sensor 2 TOA Inverse radiative transfer **Direct radiative** (atmospheric transfer correction) Surface reflectance Surface reflectance SURFACE for reference sensor for sensor 2



#### **Geometrical coupling**



→ Necessary to perform the intercalibration with measurements acquired in the same directions (solar and viewing)



#### **Geometrical coupling conditions:**

$$\left| \frac{\theta_s^{CAL} - \theta_s^{REF}}{\theta_v^{CAL} - \theta_v^{REF}} \right| < 2^{\circ}$$

$$\left| \frac{\theta_v^{CAL} - \theta_v^{REF}}{\theta_v^{CAL}} \right| < \frac{1}{2^{\circ}}$$

$$\left| \frac{\varphi_s^{CAL} - \varphi_v^{CAL}}{\theta_v^{CAL}} \right| = \frac{1}{2^{\circ}}$$

$$\begin{aligned} \left| \theta_{s}^{CAL} - \theta_{s}^{REF} \right| < 5^{\circ} \\ \left| \theta_{v}^{CAL} - \theta_{v}^{REF} \right| < 5^{\circ} \\ \left\| \varphi_{s}^{CAL} - \varphi_{v}^{CAL} \right| - \left| \varphi_{s}^{REF} - \varphi_{v}^{REF} \right\| < 10^{\circ} \end{aligned}$$

**Objectif:** compromise between number of matched measurements and the need to avoid errors in the inter-calibration due to the bidirectional behaviour of the reflectance of the site

→ These equations implies that the BRDF is symmetric with respect to the principal plane

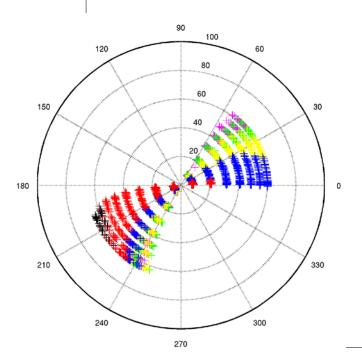
The second solution to increase matching measurements is to apply the reciprocity principle

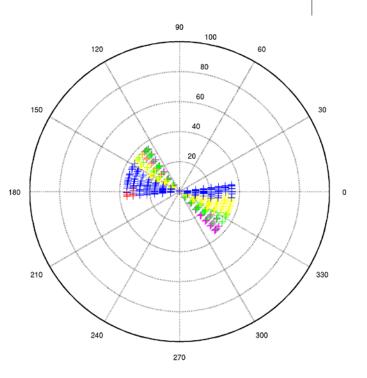


#### **Geometrical coupling conditions**

# **Example with the inter-calibration of MODIS / MERIS**

#### No matching





**MODIS SADE dataset** (1920 measurements)

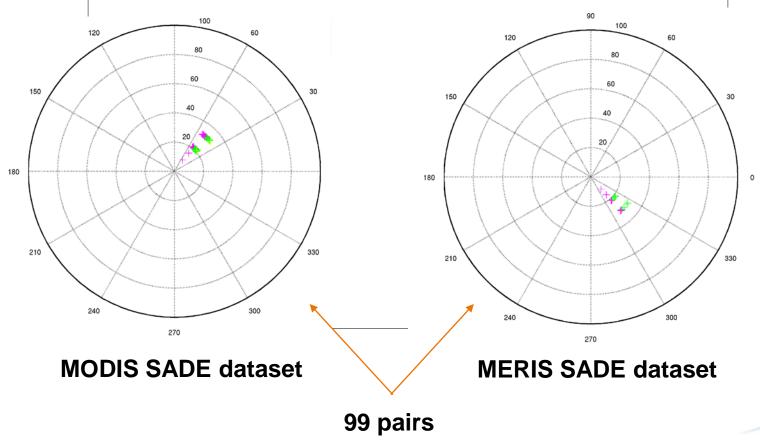
**MERIS SADE dataset** (1255 measurements)



#### **Geometrical coupling conditions**

# **Example with the inter-calibration of MODIS / MERIS**

Coupling conditions: ( $\theta$ s<2- $\theta$ v<2- $\Delta \phi$ <5) without reciprocity



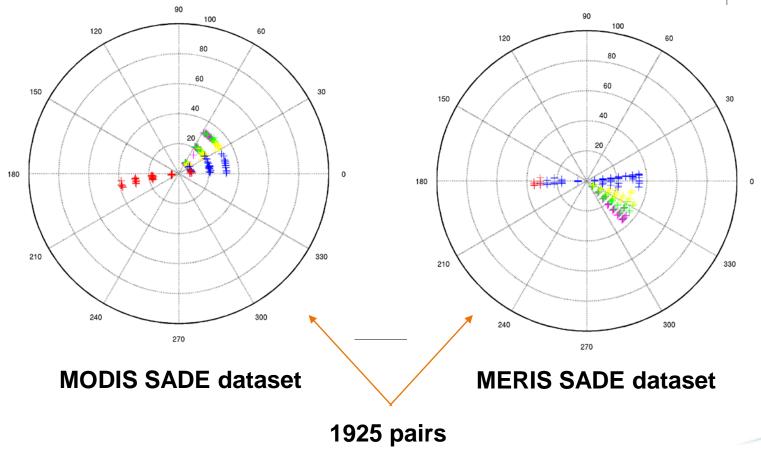


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#### **Geometrical coupling conditions**

# **Example with the inter-calibration of MODIS / MERIS**

Coupling conditions: ( $\theta s < 5 - \theta v < 5 - \Delta \phi < 10$ ) without reciprocity

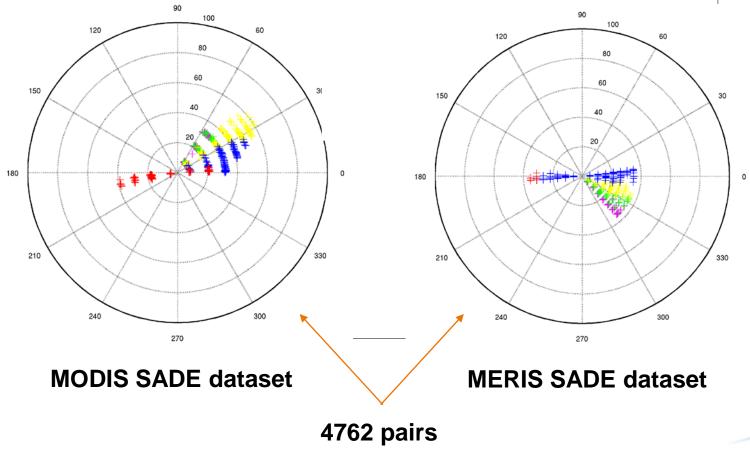




#### **Geometrical coupling conditions**

# **Example with the inter-calibration of MODIS / MERIS**

#### Coupling conditions: ( $\theta$ s<5- $\theta$ v<5- $\Delta \phi$ <10) with reciprocity





Atmospheric corrections **Cross-calibration** Comparison = Sensor 2 vs Reference Sensor  $\Delta A_{k}$ Measured Measured **Computed TOA reflectance** TOA reflectance for **TOA reflectance** for Sensor 2 Reference Sensor for Sensor 2 TOA Inverse radiative transfer **Direct radiative** (atmospheric transfer correction) Surface reflectance Surface reflectance SURFACE for reference sensor for sensor 2





- -Inverse radiative transfer
- → To derive the BOA reflectance for the reference sensor
- -Direct radiative transfer
- → A direct computation to obtain the simulated TOA reflectance of the reference sensor in the sensor spectral bands to calibrate
- -Use of SMAC to calculate the atmospheric coefficients for the two sensors
- -H20 and Pressure content from NCEP (US weather service)
  - -O3 from TOMS (OMI satellites)
  - -Aerosol: AOT = 0.2 at 550nm associated to a desertic aerosol model
    - ->This assumption (use for the direct and inverse atmospheric contribution) does not introduce a mean bias but just day to day variations



**Spectral Interpolation Cross-calibration** Comparison = Sensor 2 vs Reference Sensor  $\Delta A_{l}$ Measured Measured **Computed TOA reflectance** TOA reflectance for **TOA reflectance** for Sensor 2 Reference Sensor for Sensor 2 TOA Inverse radiative transfer **Direct radiative** (atmospheric transfer correction) Surface reflectance Surface reflectance SURFACE for reference sensor for sensor 2 **Spectral interpolation** 

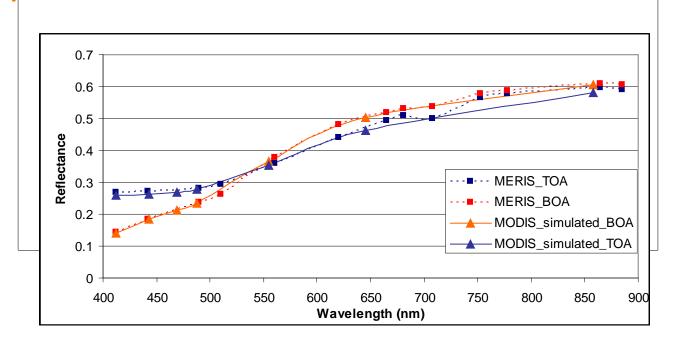




Goal: to convert the BOA reflectance of the reference sensor to the spectral bands of the sensor to calibrate

→ Use of a Spline function (smooth curve between spectral bands)

#### **Example of the calibration of MODIS versus MERIS**







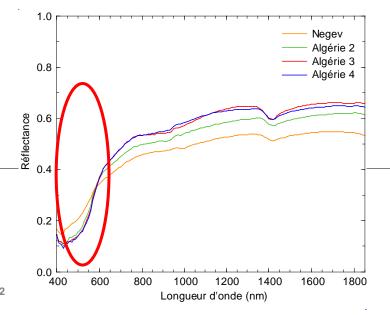
Goal: to convert the BOA reflectance of the reference sensor to the spectral bands of the sensor to calibrate

→ Use of a Spline function (smooth curve between spectral bands)

Be careful to the choice of the reference sensor regarding the spectral band to model (CAL sensor) !!!

The final accuracy is strongly linked to this adequacy

Sand reflectance measured in laboratory (ONERA)





#### Intercalibration coefficient computation

$$A_{k,CAL\_REF}(t) = \frac{1}{n} \sum_{n\_pairs} A_{k,CAL\_REF}(t) = \frac{1}{n} \sum_{n\_pairs} \frac{\rho_{k,CAL}}{\rho_{k,REF}}$$

- → Ratio is computed for each pairs of measurements of the two sensors and average over the all set of matched measurements
- → Defectuous measurements due to saturation or abnormal behavior are discarded.

#### The accuracy of this method depends on two main aspects:

- the reference sensor (spectral band coverage)
- the spatial geometrical sampling for the two sensors
- the number of matched measurements

When conditions are optimum, accuracy ~ 1% between 2 sensors, or some bands of these 2 sensors



#### **Improvement**



#### A fixed geometrical window has 2 drawbacks:

- → limit the number of measurements for low VZA whereas the bidirectional behavior of desert sites shows a very small variation
- → could lead to large errors near hot spot
- → On-going ! (see next presentation)
- Spectral interpolation step

To add an a priori on surface spectrum to help the spectral interpolation

- → on-ground measurement
- → satellite-based measurements (Hyperion or Sciamachy )
- Spectral domain: extension to SWIR bands
- Cross-calibration GEO-LEO

